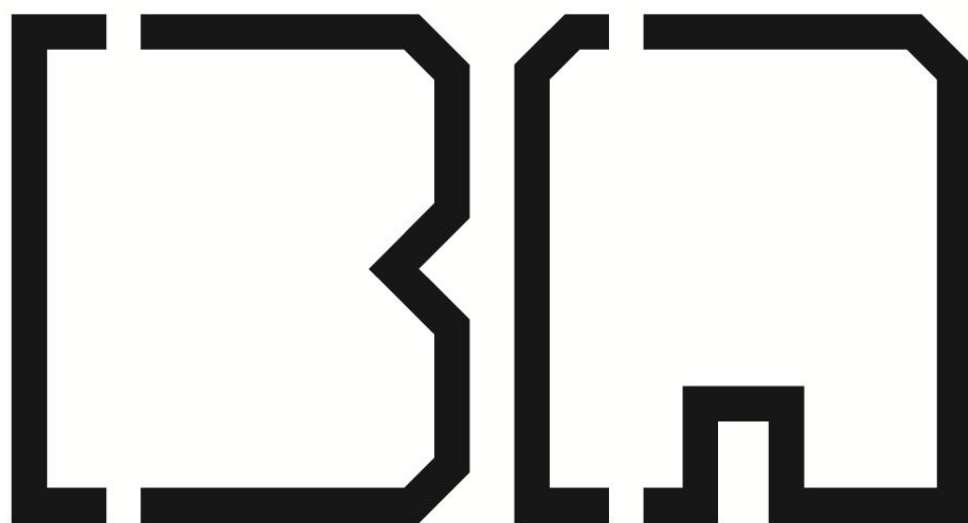


Politechnika Lubelska

Wydział Budownictwa i Architektury



Mechanika Budowli II

Projekt 1: Metoda przemieszczeń

Wykonał:

.....

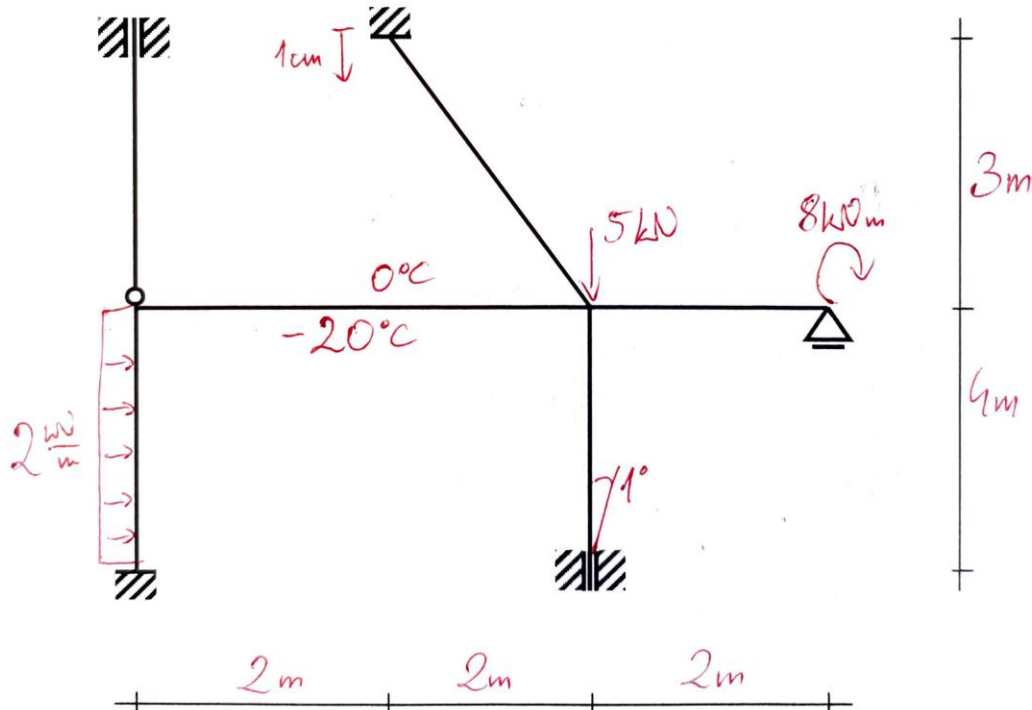
Sprawdził:

dr inż. Jakub Gontarz

ĆWICZENIE PROJEKTOWE NR 1 Z MECHANIKI BUDOWLI

PRZYKŁADOWY
TEMAT

Ramę geometrycznie niewyznaczalną rozwiązać metodą przemieszczeń.



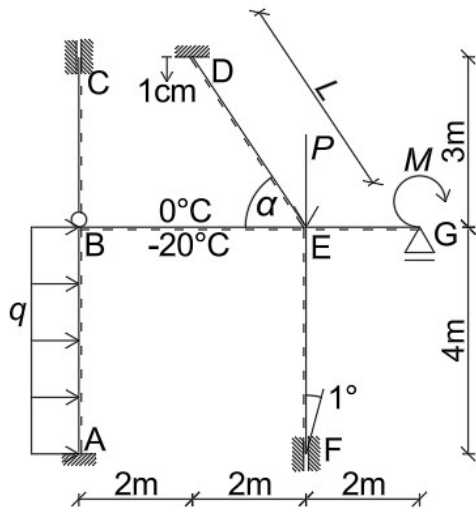
Przekrój: **I 120**

$E = 210 \text{ GPa}$

$\alpha_t = 1,2 \cdot 10^{-5} \text{ 1/K}$

G

$$\text{kNm} := \text{kN} \cdot \text{m}$$



$$E := 210 \text{ GPa}$$

$$\alpha_t := 1.2 \cdot 10^{-5} \frac{1}{\text{K}}$$

Przekrój: IPN 120

$$J := 328 \text{ cm}^4$$

$$EJ := E \cdot J = 688.8 \text{ kN} \cdot \text{m}^2$$

$$h := 120 \text{ mm}$$

Długość pręta ukośnego:

$$L := \sqrt{(2 \text{ m})^2 + (3 \text{ m})^2} = 3.606 \text{ m}$$

$$\sin \alpha := \frac{3 \text{ m}}{L} = 0.832$$

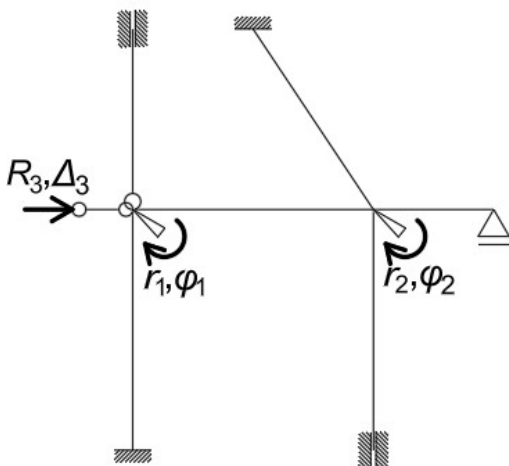
$$\cos \alpha := \frac{2 \text{ m}}{L} = 0.555$$

$$P := 5 \text{ kN}$$

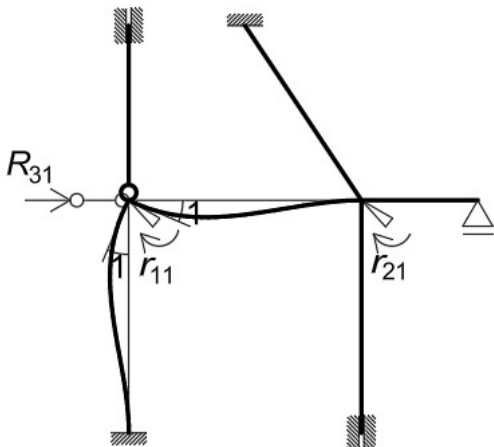
$$M := 8 \text{ kNm}$$

$$q := 2 \frac{\text{kN}}{\text{m}}$$

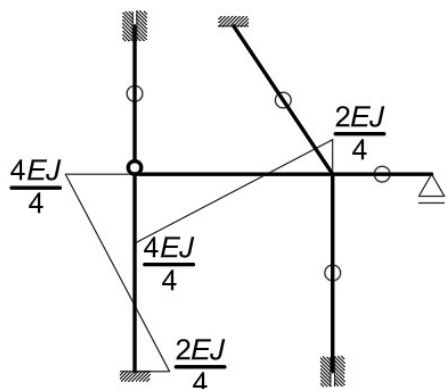
UPMP



Stan 1

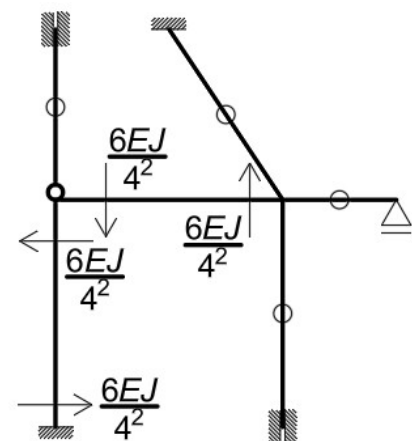


M1 [kNm]



$$M_1 := \begin{bmatrix} \frac{2 EJ}{4 \text{ m}} & \frac{-4 EJ}{4 \text{ m}} \\ 0 & 0 \\ \frac{4 EJ}{4 \text{ m}} & \frac{-2 EJ}{4 \text{ m}} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} 344.4 & -688.8 \\ 0 & 0 \\ 688.8 & -344.4 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \text{ kNm}$$

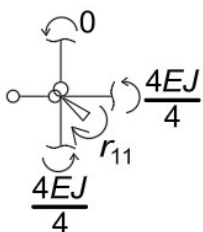
T1 [kN]



$$T_1 := \begin{bmatrix} \frac{-6 EJ}{(4 \text{ m})^2} & \frac{-6 EJ}{(4 \text{ m})^2} \\ 0 & 0 \\ \frac{-6 EJ}{(4 \text{ m})^2} & \frac{-6 EJ}{(4 \text{ m})^2} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} -258.3 & -258.3 \\ 0 & 0 \\ -258.3 & -258.3 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \text{ kN}$$

Obliczenia reakcji

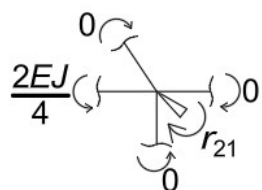
Węzeł B



$$\Sigma M = r_{11} - \frac{4 EJ}{4} - \frac{4 EJ}{4} = 0$$

$$r_{11} := \frac{4 EJ}{4 \text{ m}} + \frac{4 EJ}{4 \text{ m}} = 2 \frac{EJ}{\text{m}} \quad r_{11} = 1377.6 \text{ kNm}$$

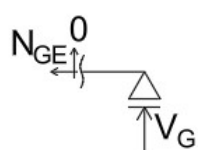
Węzeł E



$$\Sigma M = r_{21} - \frac{2 EJ}{4} = 0$$

$$r_{21} := \frac{2 EJ}{4 \text{ m}} = 0.5 \frac{EJ}{\text{m}} \quad r_{21} = 344.4 \text{ kNm}$$

Węzeł G



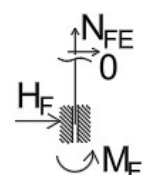
$$\Sigma X = -N_{GE} = 0$$

$$N_{GE} := 0$$

$$N_{EG} := N_{GE}$$

Siła N jest równa 0 w tym przecie
we wszystkich stanach

Węzeł F



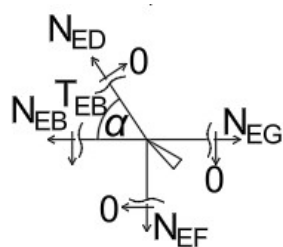
$$\Sigma Y = N_{FE} = 0$$

$$N_{FE} := 0$$

$$N_{EF} := N_{FE}$$

Siła N jest równa 0 w tym przecie
we wszystkich stanach

Węzeł E



$$T_{EB} := \frac{6 EJ}{(4 \text{ m})^2}$$

$$\Sigma Y = -N_{EF} - T_{EB} + N_{ED} \cdot \sin \alpha = 0$$

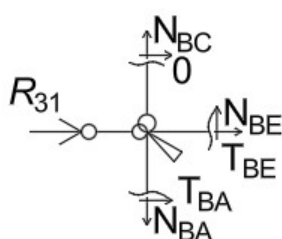
$$N_{ED} := \frac{N_{EF} + T_{EB}}{\sin \alpha} = 0.451 \frac{EJ}{\text{m}^2}$$

$$\Sigma X = -N_{EB} + N_{EG} - N_{ED} \cdot \cos \alpha = 0$$

$$N_{EB} := N_{EG} - N_{ED} \cdot \cos \alpha = -0.25 \frac{EJ}{\text{m}^2}$$

$$N_{BE} := N_{EB}$$

Węzeł B



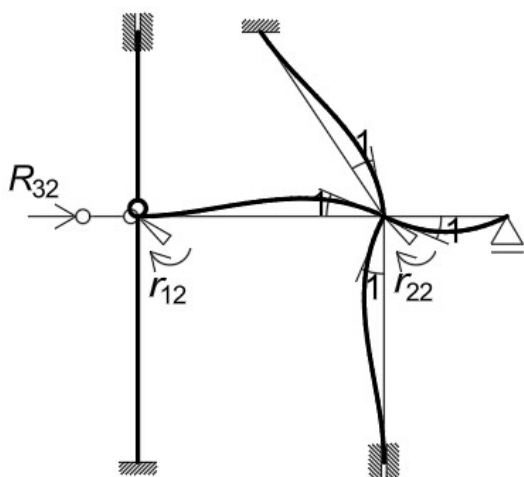
$$T_{BA} := \frac{6 EJ}{(4 \text{ m})^2}$$

$$\Sigma X = R_{31} + N_{BE} + T_{BA} = 0$$

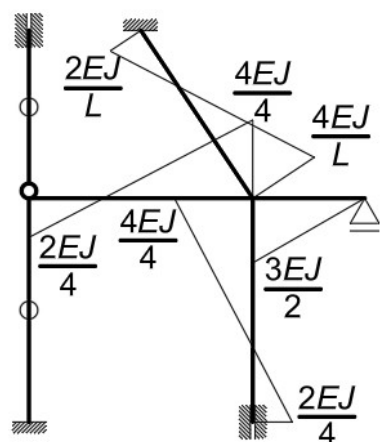
$$R_{31} := -N_{BE} - T_{BA} = -0.125 \frac{EJ}{\text{m}^2}$$

$$R_{31} = -86.1 \text{ kN}$$

Stan 2

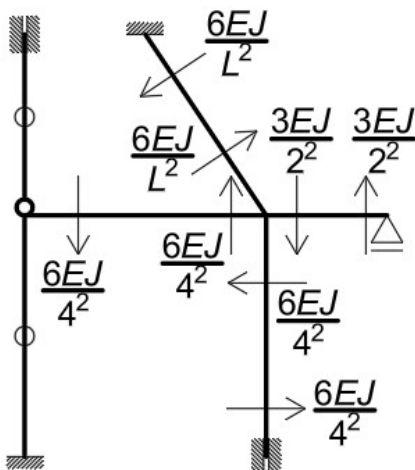


M2 [kN]



$$M_2 := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{2 EJ}{4 \text{ m}} & \frac{-4 EJ}{4 \text{ m}} \\ \frac{2 EJ}{L} & \frac{-4 EJ}{L} \\ \frac{4 EJ}{4 \text{ m}} & \frac{-2 EJ}{4 \text{ m}} \\ \frac{3 EJ}{2 \text{ m}} & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 344.4 & -688.8 \\ 382.077 & -764.155 \\ 688.8 & -344.4 \\ 1033.2 & 0 \end{bmatrix} \text{ kNm}$$

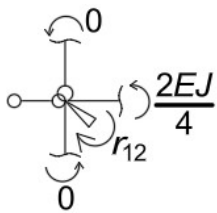
T2 [kN/m]



$$T_2 := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{-6 EJ}{(4 \text{ m})^2} & \frac{-6 EJ}{(4 \text{ m})^2} \\ \frac{-6 EJ}{L^2} & \frac{-6 EJ}{L^2} \\ \frac{-6 EJ}{(4 \text{ m})^2} & \frac{-6 EJ}{(4 \text{ m})^2} \\ \frac{-3 EJ}{(2 \text{ m})^2} & \frac{-3 EJ}{(2 \text{ m})^2} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ -258.3 & -258.3 \\ -317.908 & -317.908 \\ -258.3 & -258.3 \\ -516.6 & -516.6 \end{bmatrix} \text{ kN}$$

Obliczenia reakcji

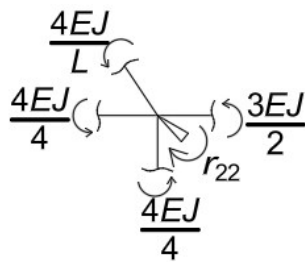
Węzeł B



$$\sum M = r_{12} - \frac{2 EJ}{4} = 0$$

$$r_{12} := \frac{2 EJ}{4 \text{ m}} = 0.5 \frac{EJ}{\text{m}} \quad r_{12} = 344.4 \text{ kNm}$$

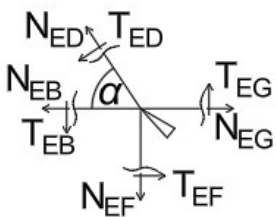
Węzeł E



$$\sum M = r_{22} - \frac{4 EJ}{4} - \frac{4 EJ}{4} - \frac{3 EJ}{2} - \frac{4 EJ}{L} = 0$$

$$r_{22} := \frac{4 EJ}{4 \text{ m}} + \frac{4 EJ}{4 \text{ m}} + \frac{3 EJ}{2 \text{ m}} + \frac{4 EJ}{L} = 4.609 \frac{EJ}{\text{m}} \quad r_{22} = 3174.955 \text{ kNm}$$

Węzeł E



$$T_{EB} := \frac{6 EJ}{(4 \text{ m})^2} \quad T_{ED} := \frac{6 EJ}{L^2} \quad T_{EF} := \frac{6 EJ}{(4 \text{ m})^2} \quad T_{EG} := \frac{3 EJ}{(2 \text{ m})^2}$$

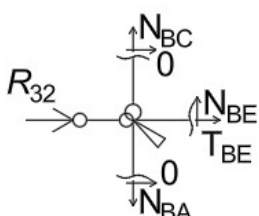
$$\sum Y = -N_{EF} - T_{EB} + T_{EG} + N_{ED} \cdot \sin \alpha - T_{ED} \cdot \cos \alpha = 0$$

$$N_{ED} := \frac{N_{EF} + T_{EB} - T_{EG} + T_{ED} \cdot \cos \alpha}{\sin \alpha} = -0.143 \frac{EJ}{\text{m}^2}$$

$$\sum X = -N_{EB} + N_{EG} - N_{ED} \cdot \cos \alpha - T_{ED} \cdot \sin \alpha + T_{EF} = 0$$

$$N_{EB} := N_{EG} - N_{ED} \cdot \cos \alpha - T_{ED} \cdot \sin \alpha + T_{EF} = 0.07 \frac{EJ}{\text{m}^2} \quad N_{BE} := N_{EB}$$

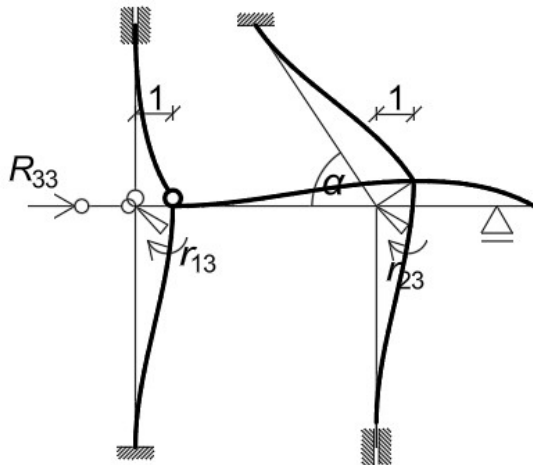
Węzeł B



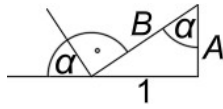
$$\sum X = R_{32} + N_{BE} = 0$$

$$R_{32} := -N_{BE} = -0.07 \frac{EJ}{\text{m}^2} \quad R_{32} = -48.423 \text{ kN}$$

Stan 3



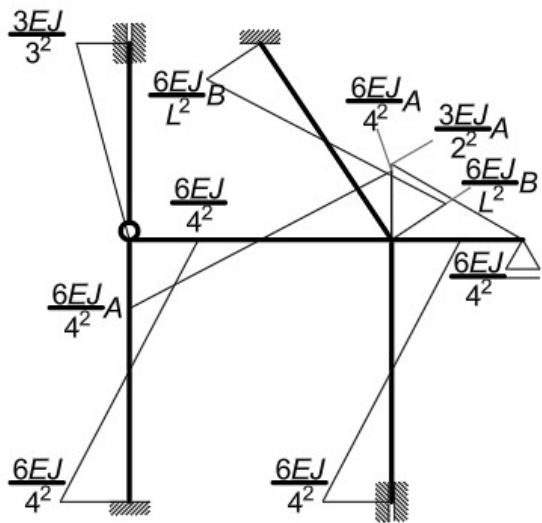
Obliczenie proporcji:



$$A := \frac{2 \text{ m}}{3 \text{ m}} = 0.667$$

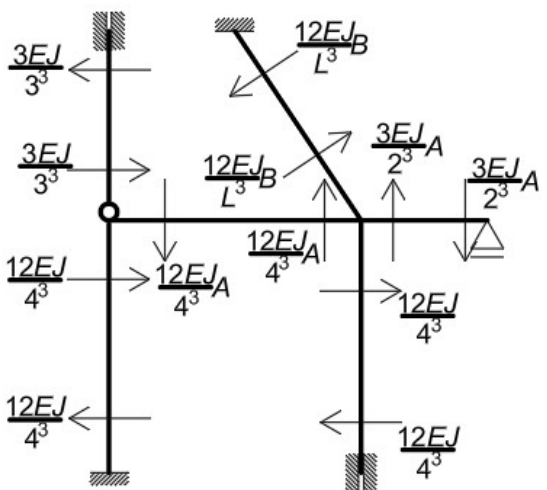
$$B := \frac{L}{3 \text{ m}} = 1.202$$

M3 [kN]



$$M_3 := \begin{bmatrix} \frac{-6 EJ}{(4 \text{ m})^2} & \frac{6 EJ}{(4 \text{ m})^2} \\ 0 & \frac{-3 EJ}{(3 \text{ m})^2} \\ \frac{6 EJ}{(4 \text{ m})^2} A & \frac{-6 EJ}{(4 \text{ m})^2} A \\ \frac{6 EJ}{L^2} B & \frac{-6 EJ}{L^2} B \\ \frac{-6 EJ}{(4 \text{ m})^2} & \frac{6 EJ}{(4 \text{ m})^2} \\ \frac{-3 EJ}{(2 \text{ m})^2} A & 0 \end{bmatrix} = ? \text{ kN}$$

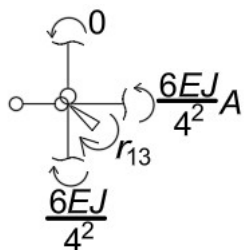
T3 [kN/m]



$$T_3 := \begin{bmatrix} \frac{12 EJ}{(4 \text{ m})^3} & \frac{12 EJ}{(4 \text{ m})^3} \\ \frac{-3 EJ}{(3 \text{ m})^3} & \frac{-3 EJ}{(3 \text{ m})^3} \\ \frac{-12 EJ}{(4 \text{ m})^3} A & \frac{-12 EJ}{(4 \text{ m})^3} A \\ \frac{-12 EJ}{L^3} B & \frac{-12 EJ}{L^3} B \\ \frac{12 EJ}{(4 \text{ m})^3} & \frac{12 EJ}{(4 \text{ m})^3} \\ \frac{3 EJ}{(2 \text{ m})^3} A & \frac{3 EJ}{(2 \text{ m})^3} A \end{bmatrix} = \begin{bmatrix} 129.15 & 129.15 \\ -76.533 & -76.533 \\ -86.1 & -86.1 \\ -211.938 & -211.938 \\ 129.15 & 129.15 \\ 172.2 & 172.2 \end{bmatrix} \frac{\text{kN}}{\text{m}}$$

Obliczenia reakcji

Węzeł B

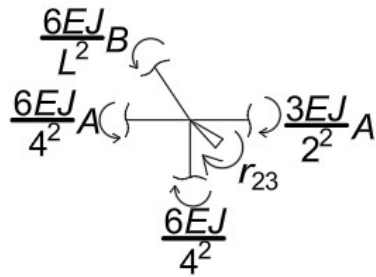


$$\Sigma M = r_{13} - \frac{6 EJ}{4^2} \cdot A + \frac{6 EJ}{4^2} = 0$$

$$r_{13} := \frac{6 EJ}{(4 \text{ m})^2} \cdot A - \frac{6 EJ}{(4 \text{ m})^2} = -0.125 \frac{EJ}{\text{m}^2}$$

$$r_{13} = -86.1 \text{ kN}$$

Węzeł E

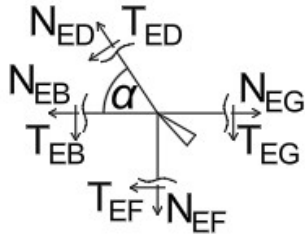


$$\Sigma M = r_{22} - \frac{6 EJ}{L^2} \cdot B - \frac{6 EJ}{4^2} \cdot A + \frac{6 EJ}{4^2} + \frac{3 EJ}{2^2} \cdot A = 0$$

$$r_{23} := \frac{6 EJ}{L^2} \cdot B + \frac{6 EJ}{(4 \text{ m})^2} \cdot A - \frac{6 EJ}{(4 \text{ m})^2} - \frac{3 EJ}{(2 \text{ m})^2} \cdot A = -0.07 \frac{EJ}{\text{m}^2}$$

$$r_{23} = -48.423 \text{ kN}$$

Węzeł E



$$T_{EB} := \frac{12 EJ}{(4 \text{ m})^3} A$$

$$T_{ED} := \frac{12 EJ}{L^3} B$$

$$T_{EF} := \frac{12 EJ}{(4 \text{ m})^3}$$

$$T_{EG} := \frac{3 EJ}{(2 \text{ m})^3} A$$

$$T_{BC} := \frac{3 EJ}{(3 \text{ m})^3}$$

$$T_{BA} := \frac{12 EJ}{(4 \text{ m})^3}$$

$$\Sigma Y = -N_{EF} - T_{EB} - T_{EG} + N_{ED} \cdot \sin \alpha - T_{ED} \cdot \cos \alpha = 0$$

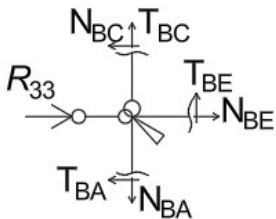
$$N_{ED} := \frac{N_{EF} + T_{EB} + T_{EG} + T_{ED} \cdot \cos \alpha}{\sin \alpha} = 0.656 \frac{EJ}{\text{m}^3}$$

$$\Sigma X = -N_{EB} + N_{EG} - N_{ED} \cdot \cos \alpha - T_{ED} \cdot \sin \alpha - T_{EF} = 0$$

$$N_{EB} := N_{EG} - N_{ED} \cdot \cos \alpha - T_{ED} \cdot \sin \alpha - T_{EF} = -0.807 \frac{EJ}{\text{m}^3}$$

$$N_{BE} := N_{EB}$$

Węzeł B

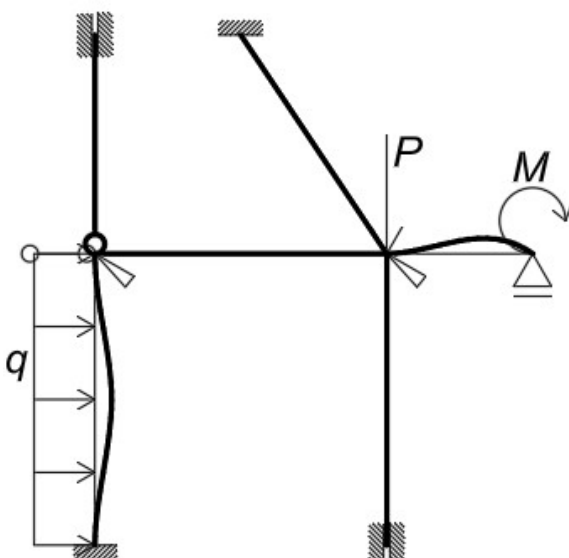


$$\Sigma X = R_{33} + N_{BE} - T_{BC} - T_{BA} = 0$$

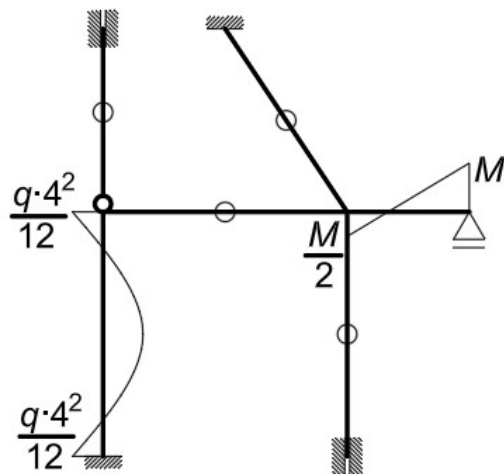
$$R_{33} := -N_{BE} + T_{BC} + T_{BA} = 1.106 \frac{EJ}{\text{m}^3}$$

$$R_{33} = 761.752 \frac{\text{kN}}{\text{m}}$$

Stan p

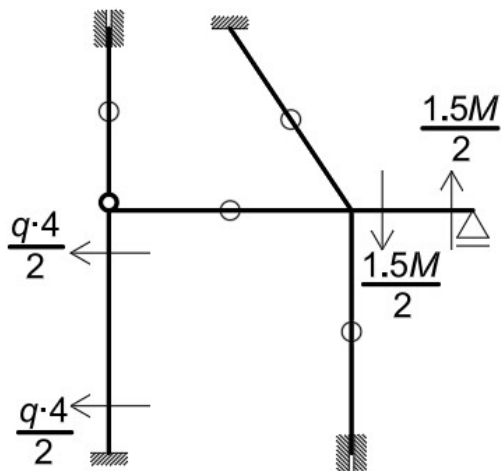


Mp [kNm]



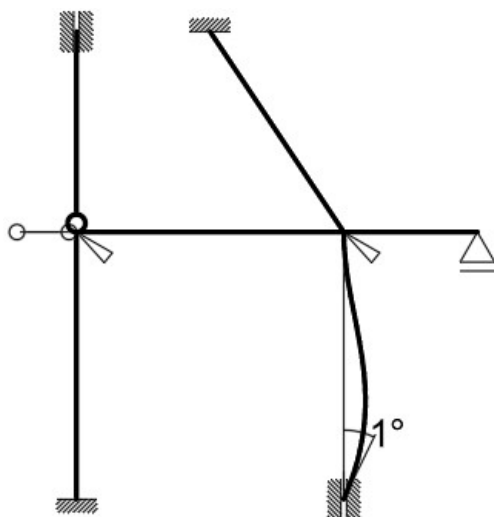
$$M_p := \begin{bmatrix} \frac{-q \cdot (4 \text{ m})^2}{12} & \frac{-q \cdot (4 \text{ m})^2}{12} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{M}{2} & -M \end{bmatrix} = \begin{bmatrix} -2.667 & -2.667 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 4 & -8 \end{bmatrix} \text{ kNm}$$

Tp [kN]

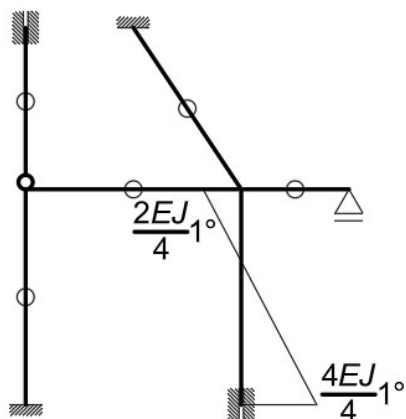


$$T_p := \begin{bmatrix} \frac{q \cdot 4 \text{ m}}{2} & \frac{-q \cdot 4 \text{ m}}{2} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{-1.5 M}{2 \text{ m}} & \frac{-1.5 M}{2 \text{ m}} \end{bmatrix} = \begin{bmatrix} 4 & -4 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ -6 & -6 \end{bmatrix} \text{ kN}$$

Stan φ

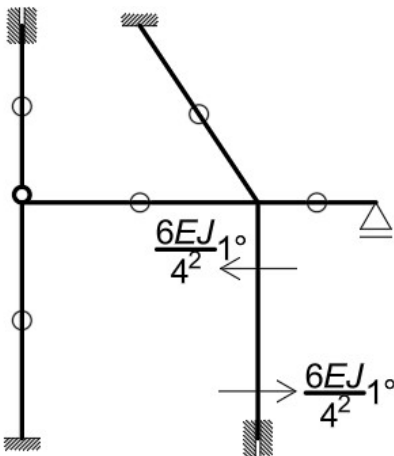


M_φ [kNm]



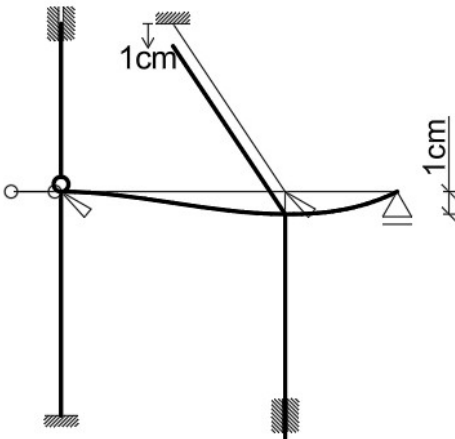
$$M_\varphi := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{2 EJ}{4 \text{ m}} 1^\circ & \frac{-4 EJ}{4 \text{ m}} 1^\circ \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 6.011 & -12.022 \\ 0 & 0 \end{bmatrix} \text{ kNm}$$

T_φ [kN]

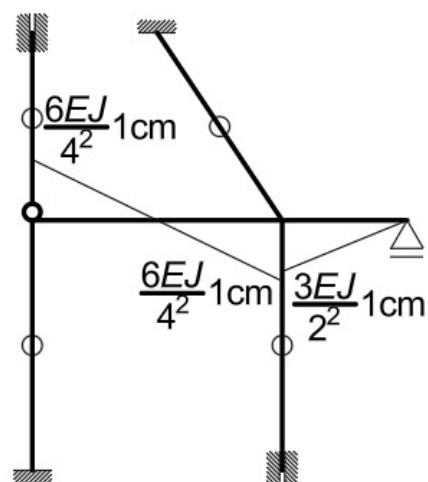


$$T_\varphi := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{-6 EJ}{(4 \text{ m})^2} 1^\circ & \frac{-6 EJ}{(4 \text{ m})^2} 1^\circ \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ -4.508 & -4.508 \\ 0 & 0 \end{bmatrix} \text{ kN}$$

Stan Δ



M_Δ [kNm]



$$M_\Delta := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \frac{-6 EJ}{(4 \text{ m})^2} 1 \text{ cm} & \frac{6 EJ}{(4 \text{ m})^2} 1 \text{ cm} \\ \frac{3 EJ}{(2 \text{ m})^2} 1 \text{ cm} & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ -2.583 & 2.583 \\ 5.166 & 0 \end{bmatrix} \text{ kNm}$$

$$T_{\Delta} := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{12 EJ}{(4 \text{ m})^3} 1 \text{ cm} & \frac{12 EJ}{(4 \text{ m})^3} 1 \text{ cm} \\ 0 & 0 \\ 0 & 0 \\ \frac{-3 EJ}{(2 \text{ m})^3} 1 \text{ cm} & \frac{-3 EJ}{(2 \text{ m})^3} 1 \text{ cm} \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1.292 & 1.292 \\ 0 & 0 \\ 0 & 0 \\ -2.583 & -2.583 \end{bmatrix} \text{ kN}$$

$$t_0 := \frac{20 \text{ K} + 0 \text{ K}}{2} = 10 \text{ K}$$

$$\frac{A}{\Delta L} = \frac{2 \text{ m}}{3 \text{ m}}$$

$$A := \frac{2 \text{ m}}{3 \text{ m}} \Delta L = 0.00032 \text{ m}$$

$$\frac{B}{\Delta L} = \frac{L}{3 \text{ m}}$$

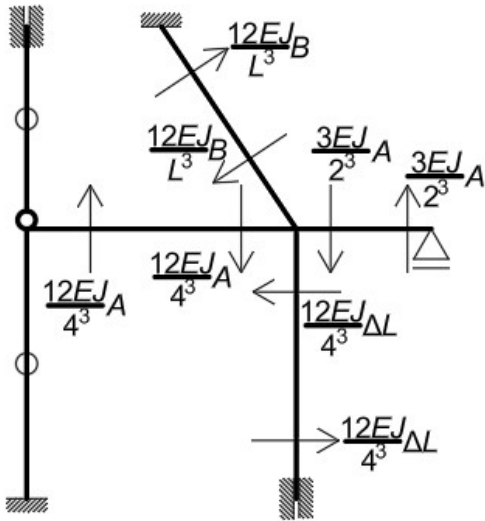
$$B := \frac{L}{3 \text{ m}} \Delta L = 0.000577 \text{ m}$$

Diagram illustrating a frame structure with various fixed-end moments and displacements. The structure consists of a vertical member on the left, a horizontal member in the middle, and a vertical member on the right. The left vertical member is fixed at the bottom and has a hinge at the top. The right vertical member is fixed at the bottom. The horizontal member is connected to both vertical members. The labels indicate the following values:

- Fixed-end moment at the top of the left vertical member: $\frac{6EJ}{4^2}A$
- Fixed-end moment at the bottom of the left vertical member: $\frac{6EJ}{L^2}B$
- Fixed-end moment at the top of the right vertical member: $\frac{6EJ}{L^2}B$
- Fixed-end moment at the bottom of the right vertical member: $\frac{6EJ}{4^2}\Delta L$
- Fixed-end moment at the left end of the horizontal member: $\frac{6EJ}{4^2}\Delta L$
- Fixed-end moment at the right end of the horizontal member: $\frac{3EJ}{2^2}A$
- Fixed-end moment at the right end of the horizontal member: $\frac{6EJ}{4^2}A$
- Fixed-end moment at the bottom of the right vertical member: $\frac{6EJ}{4^2}\Delta L$

$$M_{t0} := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{-6 EJ}{(4 \text{ m})^2} A & \frac{6 EJ}{(4 \text{ m})^2} A \\ \frac{-6 EJ}{L^2} B & \frac{6 EJ}{L^2} B \\ \frac{6 EJ}{(4 \text{ m})^2} \Delta L & \frac{-6 EJ}{(4 \text{ m})^2} \Delta L \\ \frac{3 EJ}{(2 \text{ m})^2} A & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ -0.083 & 0.083 \\ -0.183 & 0.183 \\ 0.124 & -0.124 \\ 0.165 & 0 \end{bmatrix} \text{ kNm}$$

Tt0 [kNm]

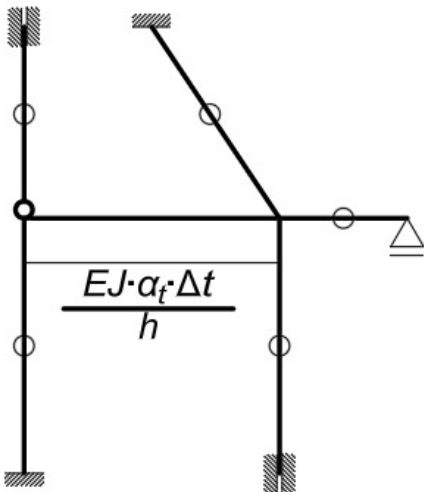


$$T_{t0} := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{12 EJ}{(4 \text{ m})^3} A & \frac{12 EJ}{(4 \text{ m})^3} A \\ \frac{12 EJ}{L^3} B & \frac{12 EJ}{L^3} B \\ -\frac{12 EJ}{(4 \text{ m})^3} \Delta L & -\frac{12 EJ}{(4 \text{ m})^3} \Delta L \\ \frac{-3 EJ}{(2 \text{ m})^3} A & \frac{-3 EJ}{(2 \text{ m})^3} A \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0.041 & 0.041 \\ 0.102 & 0.102 \\ -0.062 & -0.062 \\ -0.083 & -0.083 \end{bmatrix} \text{ kN}$$

Stan Δt

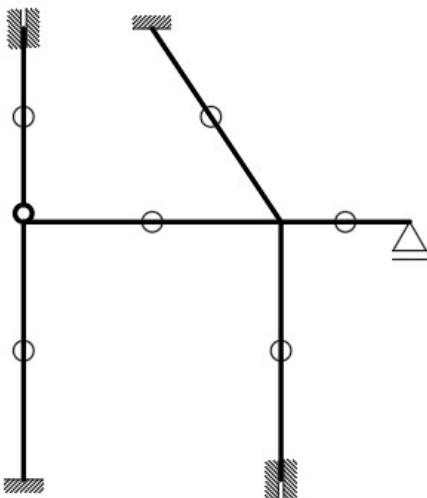
$$\Delta t := |20 \text{ K} - 0 \text{ K}| = 20 \text{ K}$$

M Δt [kNm]



$$M_{\Delta t} := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{EJ \cdot \alpha_t \cdot \Delta t}{h} & \frac{EJ \cdot \alpha_t \cdot \Delta t}{h} \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 1.378 & 1.378 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \text{ kNm}$$

T Δt [kN]

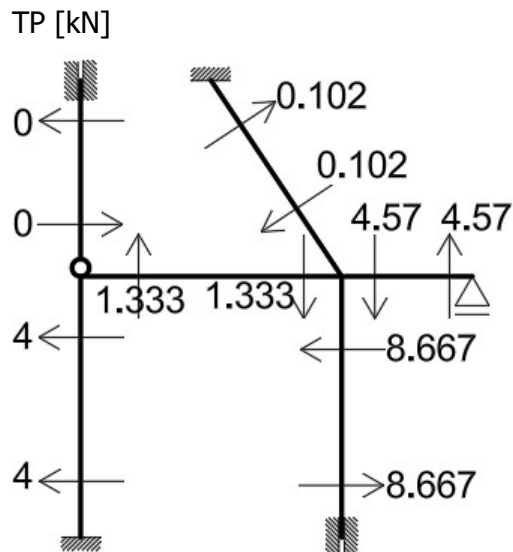
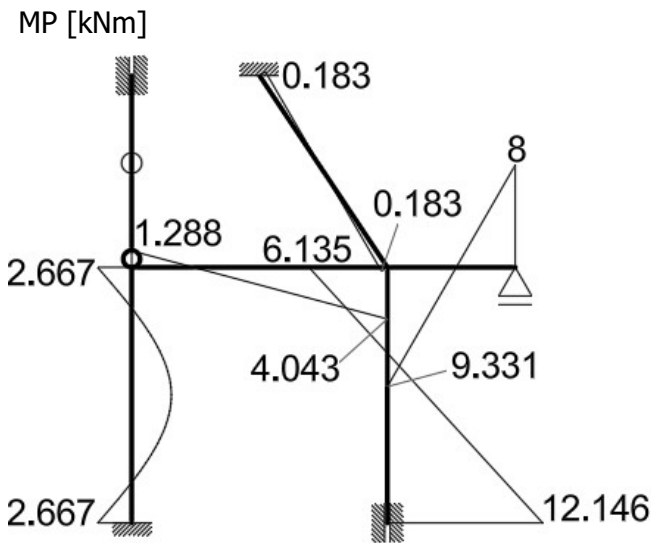


$$T_{\Delta t} := \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \text{ kN} = \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \text{ kN}$$

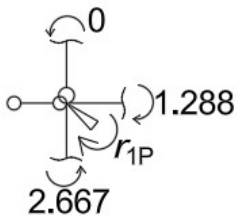
Stan rzeczywisty zsumowany:

$$M_P := M_p + M_\varphi + M_\Delta + M_{t0} + M_{\Delta t} = \begin{bmatrix} -2.667 & -2.667 \\ 0 & 0 \\ -1.288 & 4.043 \\ -0.183 & 0.183 \\ 6.135 & -12.146 \\ 9.331 & -8 \end{bmatrix} \text{ kNm}$$

$$T_P := T_p + T_\varphi + T_\Delta + T_{t0} + T_{\Delta t} = \begin{bmatrix} 4 & -4 \\ 0 & 0 \\ 1.333 & 1.333 \\ 0.102 & 0.102 \\ -4.57 & -4.57 \\ -8.666 & -8.666 \end{bmatrix} \text{ kN}$$



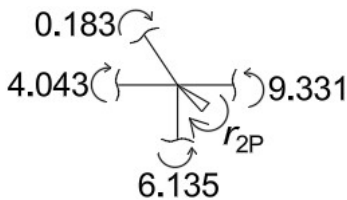
Węzeł B



$$\sum M = r_{1P} - 2.667 \text{ kNm} + 1.288 \text{ kNm} = 0$$

$$r_{1P} := 2.667 \text{ kNm} - 1.288 \text{ kNm} = 1.379 \text{ kNm}$$

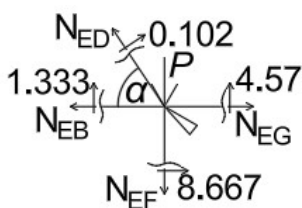
Węzeł E



$$\sum M = r_{2P} + 4.043 \text{ kNm} + 0.183 \text{ kNm} - 6.135 \text{ kNm} - 9.331 \text{ kNm} = 0$$

$$r_{2P} := -4.043 \text{ kNm} - 0.183 \text{ kNm} + 6.135 \text{ kNm} + 9.331 \text{ kNm} = 11.24 \text{ kNm}$$

Węzeł E



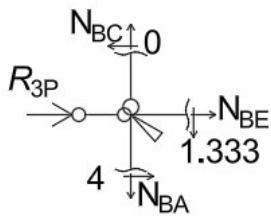
$$\sum Y = 1.333 \text{ kN} + 8.666 \text{ kN} - N_{EF} + N_{ED} \cdot \sin \alpha + 0.102 \text{ kN} \cdot \cos \alpha - 5 \text{ kN} = 0$$

$$N_{ED} := \frac{-1.333 \text{ kN} - 8.666 \text{ kN} + N_{EF} - 0.102 \text{ kN} \cdot \cos \alpha + 5 \text{ kN}}{\sin \alpha} = -6.076 \text{ kN}$$

$$\sum X = -N_{EB} + N_{EG} - N_{ED} \cdot \cos \alpha + 0.102 \text{ kN} \cdot \sin \alpha + 4.57 \text{ kN} = 0$$

$$N_{EB} := N_{EG} - N_{ED} \cdot \cos \alpha + 0.102 \text{ kN} \cdot \sin \alpha + 4.57 \text{ kN} = 8.025 \text{ kN} \quad N_{BE} := N_{EB}$$

Węzeł B



$$\Sigma X = R_{3P} + N_{BE} + 4 \text{ kN} = 0$$

$$R_{3P} := -N_{BE} - 4 \text{ kN} = -12.025 \text{ kN}$$

Układ równań:

$$r_{11} \cdot \varphi_1 + r_{12} \cdot \varphi_2 + r_{13} \cdot \Delta_3 + r_{1P} = 0$$

$$r_{21} \cdot \varphi_1 + r_{22} \cdot \varphi_2 + r_{23} \cdot \Delta_3 + r_{2P} = 0$$

$$R_{31} \cdot \varphi_1 + R_{32} \cdot \varphi_2 + R_{33} \cdot \Delta_3 + R_{3P} = 0$$

Układ równań w postaci macierzowej:

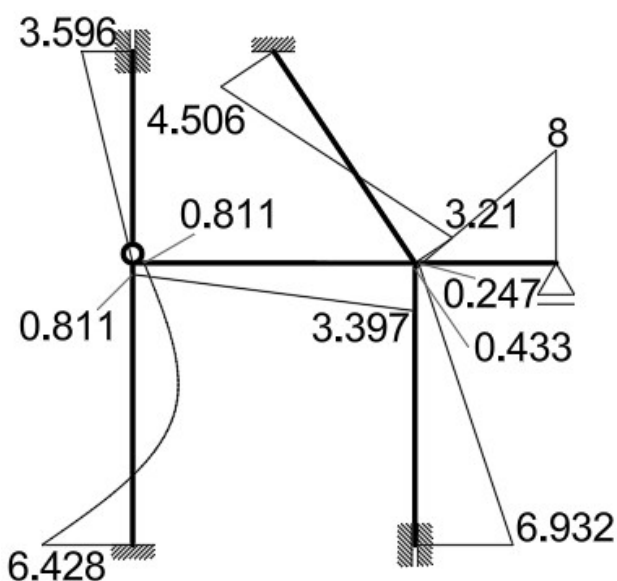
$$\begin{bmatrix} \varphi_1 \\ \varphi_2 \\ \Delta_3 \end{bmatrix} := \begin{bmatrix} r_{11} & r_{12} & r_{13} \\ r_{21} & r_{22} & r_{23} \\ R_{31} & R_{32} & R_{33} \end{bmatrix}^{-1} \cdot - \begin{bmatrix} r_{1P} \\ r_{2P} \\ R_{3P} \end{bmatrix} = \begin{bmatrix} 0.000826 \\ -0.003391 \\ 0.015664 \text{ m} \end{bmatrix}$$

Wykresy ostateczne

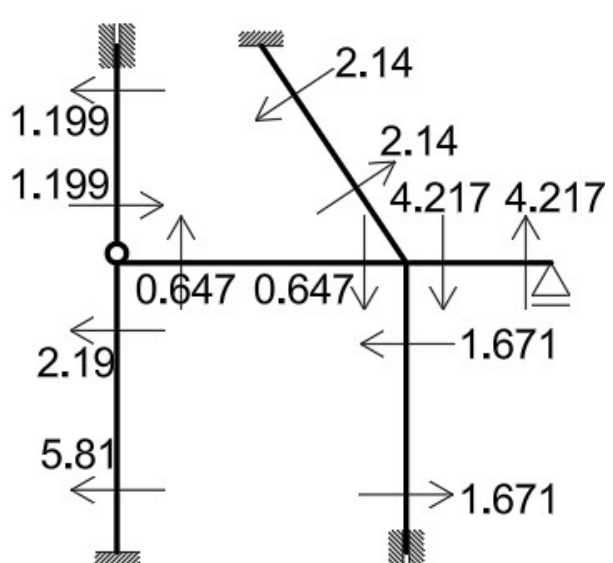
$$M_{ost} := M_1 \cdot \varphi_1 + M_2 \cdot \varphi_2 + M_3 \cdot \Delta_3 + M_P = \begin{bmatrix} -6.428 & 0.811 \\ 0 & -3.596 \\ 0.81 & 3.397 \\ 4.506 & -3.21 \\ -0.247 & -6.932 \\ 0.433 & -8 \end{bmatrix} \text{ kNm}$$

$$T_{ost} := T_1 \cdot \varphi_1 + T_2 \cdot \varphi_2 + T_3 \cdot \Delta_3 + T_P = \begin{bmatrix} 5.81 & -2.19 \\ -1.199 & -1.199 \\ 0.647 & 0.647 \\ -2.14 & -2.14 \\ -1.671 & -1.671 \\ -4.217 & -4.217 \end{bmatrix} \text{ kN}$$

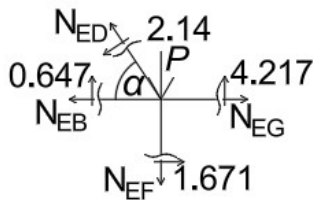
Most [kNm]



Tost [kN]



Węzeł E



$$\Sigma Y = 0.647 \text{ kN} + 4.217 \text{ kN} - N_{EF} + N_{ED} \cdot \sin \alpha - 2.14 \text{ kN} \cdot \cos \alpha - P = 0$$

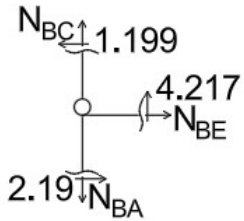
$$N_{ED} := \frac{-0.647 \text{ kN} - 4.217 \text{ kN} + N_{EF} + 2.14 \text{ kN} \cdot \cos \alpha + P}{\sin \alpha} = 1.59 \text{ kN}$$

$$\Sigma X = -N_{EB} + N_{EG} - N_{ED} \cdot \cos \alpha - 2.14 \text{ kN} \cdot \sin \alpha + 1.671 \text{ kN} = 0$$

$$N_{EB} := N_{EG} - N_{ED} \cdot \cos \alpha - 2.14 \text{ kN} \cdot \sin \alpha + 1.671 \text{ kN} = -0.992 \text{ kN}$$

$$N_{BE} := N_{EB}$$

Węzeł B



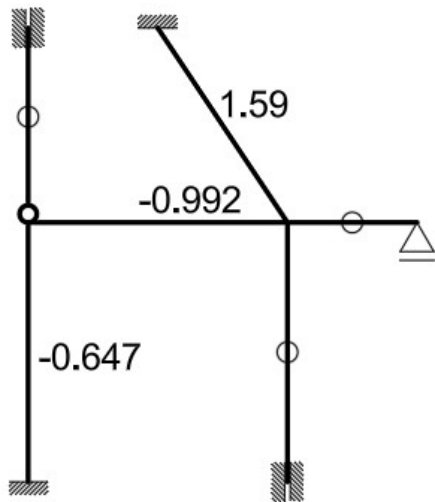
$$\Sigma Y = -0.647 \text{ kN} - N_{BA} = 0$$

$$N_{BA} := -0.647 \text{ kN}$$

Sprawdzenie:

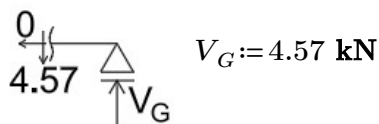
$$\Sigma X := -0.992 \text{ kN} - 1.199 \text{ kN} + 2.19 \text{ kN} = -0.001 \text{ kN}$$

Nost [kN]



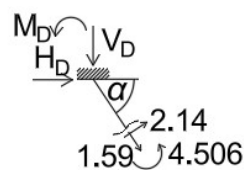
Obliczenie reakcji

Węzeł G



$$V_G := 4.57 \text{ kN}$$

Węzeł D



$$M_D := -4.506 \text{ kNm}$$

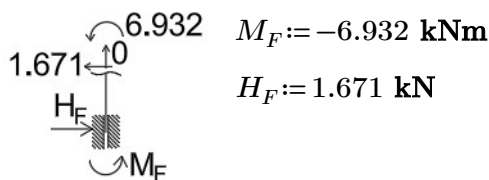
$$\Sigma X = H_D + 2.14 \text{ kN} \cdot \sin \alpha + 1.59 \text{ kN} \cdot \cos \alpha = 0$$

$$H_D := -2.14 \text{ kN} \cdot \sin \alpha - 1.59 \text{ kN} \cdot \cos \alpha = -2.663 \text{ kN}$$

$$\Sigma Y = -V_D + 2.14 \text{ kN} \cdot \cos \alpha - 1.59 \text{ kN} \cdot \sin \alpha = 0$$

$$V_D := 2.14 \text{ kN} \cdot \cos \alpha - 1.59 \text{ kN} \cdot \sin \alpha = -0.136 \text{ kN}$$

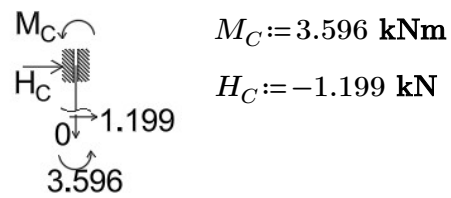
Węzeł F



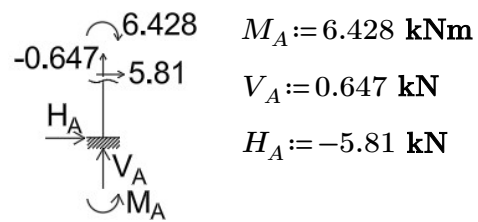
$$M_F := -6.932 \text{ kNm}$$

$$H_F := 1.671 \text{ kN}$$

Węzeł C



Węzeł A



Rost

